

# Modeling and Simulation of Space Vector Modulated Matrix Converter fed Induction Motor

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**Abstract:** Matrix Converters (MC) are reduced voltage source converters equipped for giving variable voltage variable recurrence at the yield. Contrasted and customary topologies the MC does not require a middle of the road dc interface and furnishes sinusoidal yield waveform with least higher request music. To yield higher RMS O/P voltage, it is proposed to utilize Space Vector Modulation (SVM) calculation for the voltage control of converter. This calculation utilizes a less complex technique than the other control calculations to control the info power factor. Also, it has lower exchanging misfortunes and simple execution. Reproduction has been executed for different yield frequencies at solidarity info power factor. The recreation aftereffects of yield voltage waveforms are given their spectra.

**Keywords:** Matrix Converters (MC), Space Vector Modulation (SVM), RMS O/P voltage, Rotor Speed (RPM)

## I. INTRODUCTION

The Matrix converter is the most general converter-type in the family of AC to AC direct converters. While the matrix converter fulfills the requirements to provide a sinusoidal voltage at the load side, it is also possible to adjust the unity power factor on the mains side under certain conditions. Since there is no d.c.-link as in common converters, the matrix converter can be built as a full-silicon structure (H.Altun and S.Sünter,2001). However, a mains filter is necessary to smooth the pulsed currents on the input side of the matrix converter. Using a sufficiently high pulse frequency, the output voltage and input current both are shaped sinusoidal.

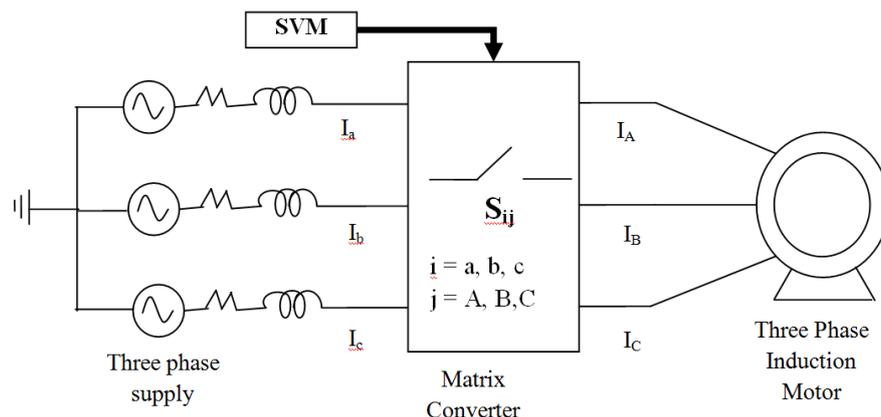


Figure 1 Matrix converter of three phase induction motor

### Space Vector Representation Of Three-Phase Variables

For a balanced three-phase sinusoidal system the instantaneous voltages are expressed as

$$\begin{bmatrix} V_{AB}(t) \\ V_{BC}(t) \\ V_{CA}(t) \end{bmatrix} = V_{01} \begin{bmatrix} \cos \omega_0 t \\ \cos(\omega_0 t - 120) \\ \cos(\omega_0 t - 240) \end{bmatrix} \quad (1)$$

This can be analyzed in terms of complex space vector

$$V_0 = \frac{2}{3} [V_{AB}(t) + V_{BC}(t)e^{j2\pi/3} + V_{CA}(t)e^{j4\pi/3}] = V_{01}e^{j\omega_0 t} \quad (2)$$

Where,  $e^{j\theta} = \cos \theta + j \sin \theta$  represents a phase shift operator and  $2/3$  is a scaling factor equal to the ratio between the magnitude of the output line-to-line voltage and that of the output voltage vector.  $\omega_0$  is the angular velocity of the vector and its magnitude is  $V_{01}$ .

Similarly, the space vector representation of the three-phase input voltage is given by

$$\vec{V}_i = V_i e^{j(\omega_i t)} \quad (3)$$

where ,

$V_i$  is the amplitude and  $\omega_i$  is the constant input angular velocity.

If a balanced three-phase load is connected to the output terminals of the converter, the space vector form of the three-phase output current and input current is given by

$$\vec{I}_0 = I_0 e^{j(\omega_0 t - \phi_0)} \quad (4)$$

$$\vec{I}_i = I_i e^{j(\omega_i t - \phi_i)} \quad (5)$$

Respectively, where  $\phi_0$  is the lagging phase angle of the output current to the output voltage and  $\phi_i$  represents the input current to the input voltage.

**Group 1** (Synchronously rotating vectors): This First group consists of six combinations in which each of the three output phases are connected to a different input phases. Each of them generates a three-phase output voltage having magnitude and frequency equivalent to those of the input voltages but with the phases sequence altered from that of the input voltages. As the input frequency is not related to the output frequency, the SVM could not use the above said vectors to synthesize the reference voltage vector that rotates at the frequency  $\omega_0$ .

**Group 2** (Stationary vectors): This second group is classified into three sets. Which has six combinations each and has a common feature of connecting two output phases to the same input phase. The corresponding vectors of these combinations have a constant phase angle. The magnitude of these vectors , however vary with changes of the instantaneous input line-line voltages.

**Group 3** (Zero vectors.): The last three combinations in the table form the last group. These have three output phases switched simultaneously on to the same input phase resulting in zero line-line voltages and are called zero voltage vectors. Output line voltage and input current space vectors are used in the application of the space vector control technique to the matrix converter.

**Selection of Stationary Vectors:** Switch combinations for matrix converter control, the SVM method is designed to choose appropriately four out of 18 switch combinations from a second group at any instant.

## II. SIMULATION MODEL

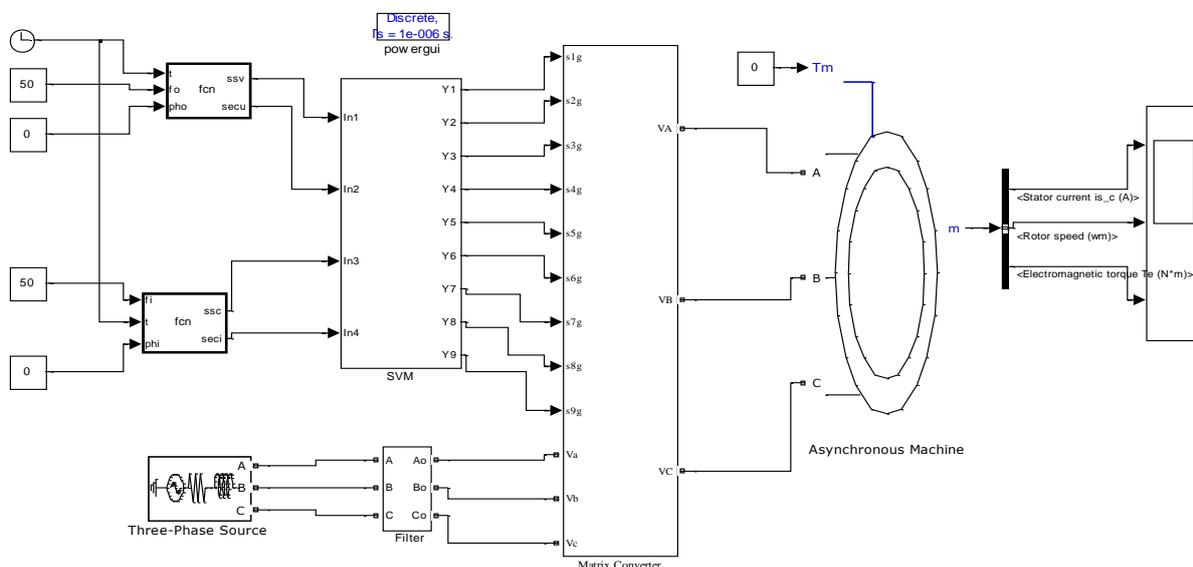


Figure 5. Simulink Model of the Controlled system

Simulation Result

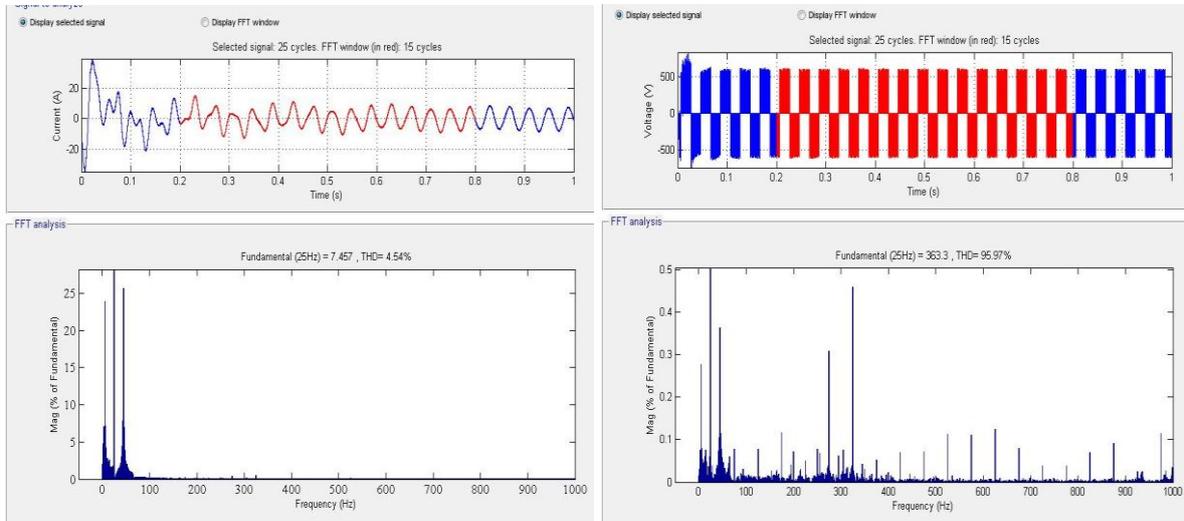


Figure 7 (a) Figure 7 (b)  
Figure 7. Matrix Converter output frequency - 100 HZ (a) Output voltage and THD (b) Output current and THD

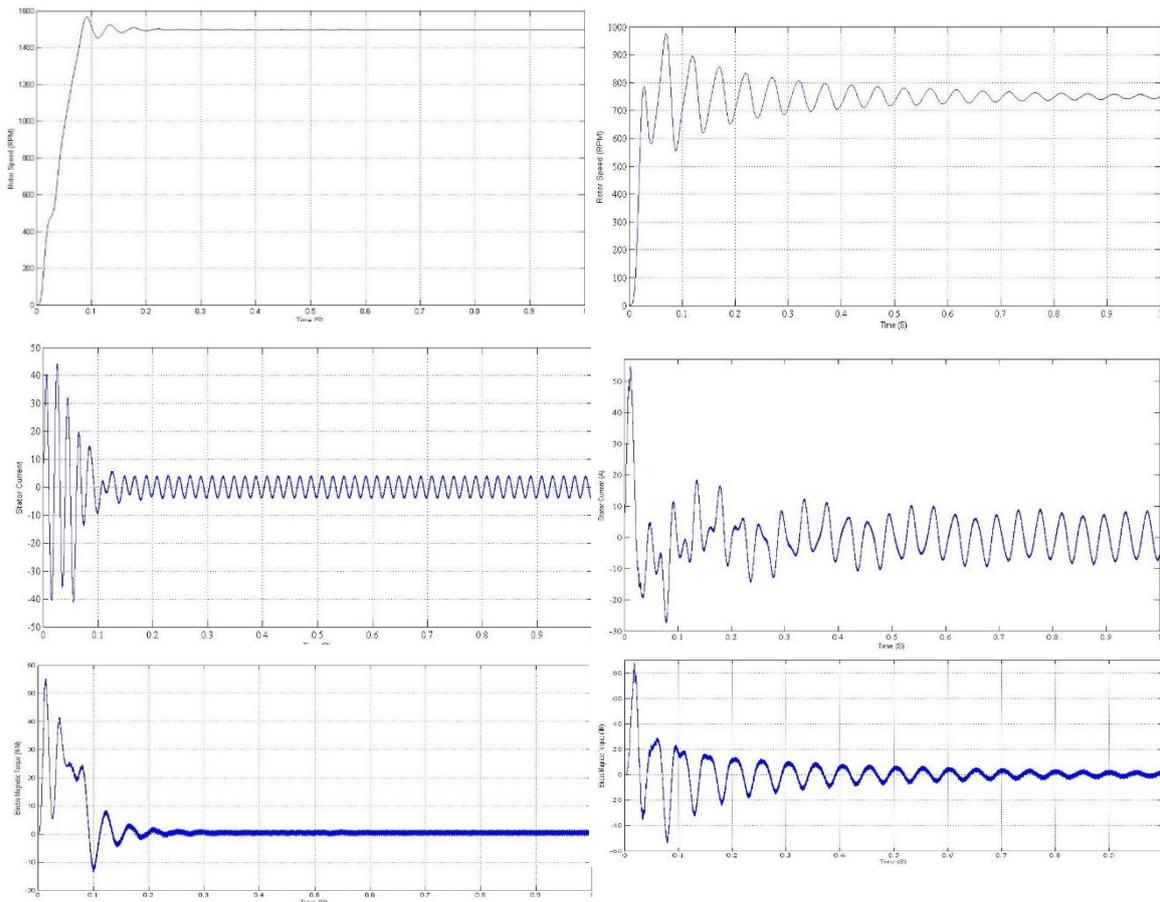


Figure 8(a) Figure 8 (b)  
Figure 8. Stator Current, Rotor Speed, Electromagnetic Torque for Matrix Converter Fed Induction Motor drive (a) 50 HZ frequency (b) 25 HZ frequency

**III. RESULT & DISCUSSION**

Table 2. Comparison statement for rotor speed and THD

Frequency (HZ)	Rotor Speed (RPM)	Matrix Converter output THD (%)	
		Current	Voltage
50	1500	3.11	95.79
25	750	4.54	95.97

The table 2 represents the comparison between two frequencies. The rotor speed were maximum in the both conditions and the THD value is also obtained for the matrix converter output voltage and current. The matrix converter response rapidly reached the maximum speed and maintained at the constant speed.

**IV. CONCLUSION**

In this investigation, displaying and recreation of the three stage Matrix Converter with Induction Motor utilizing space vector control calculation have been acknowledged in Simulink/Matlab bundle program. The information and yield waveforms of the converter for different yield frequencies have been explored. In the Simulation results exhibited over the yield waveforms did not have real music aside from those around exchanging recurrence. From the symphonious investigation, plainly the main consonant of the unfiltered input current is in stage with the information voltage.

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